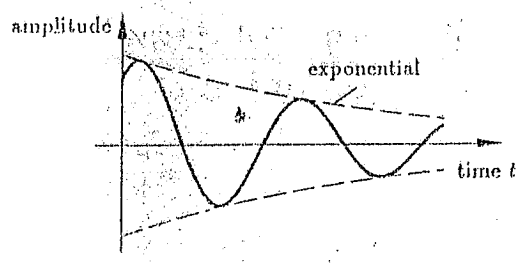
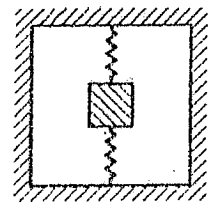
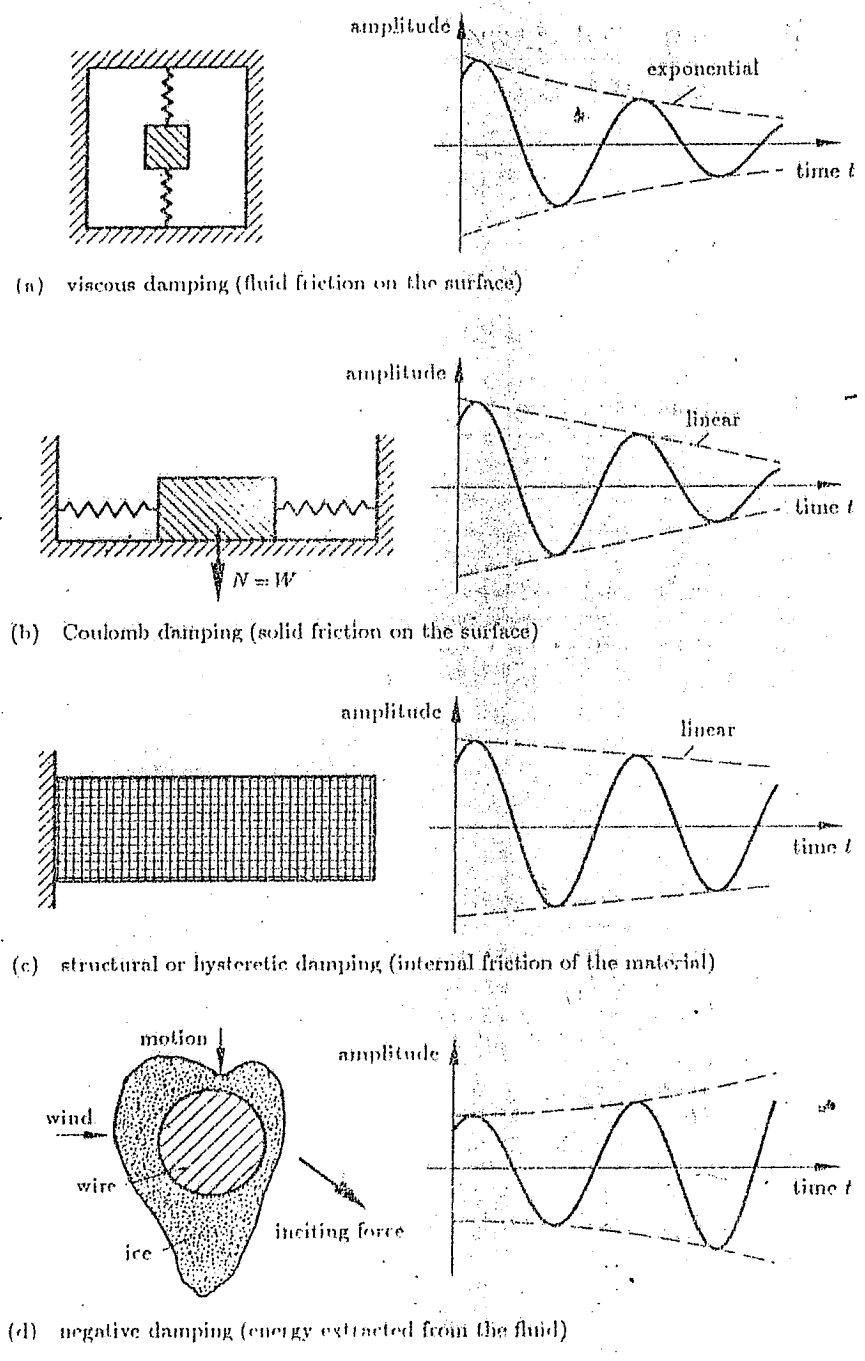
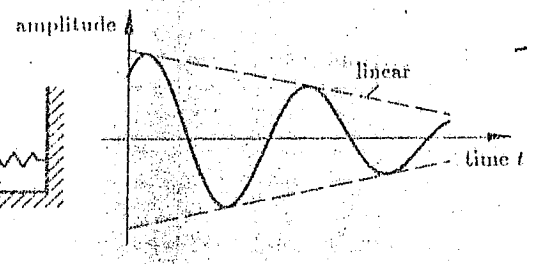
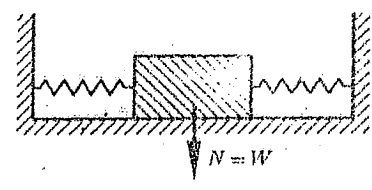


7 - Amortecimiento "Modal"

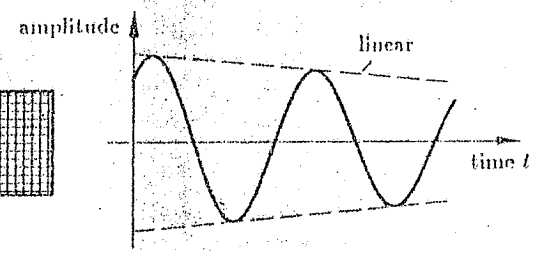
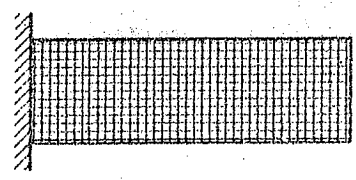
7.1) Aspectos Fenomenológicos



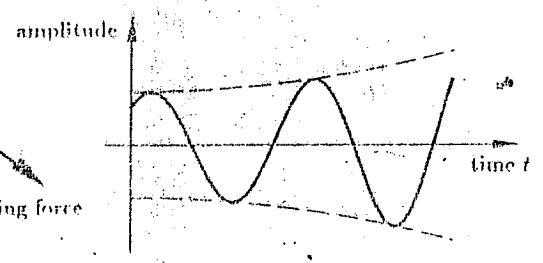
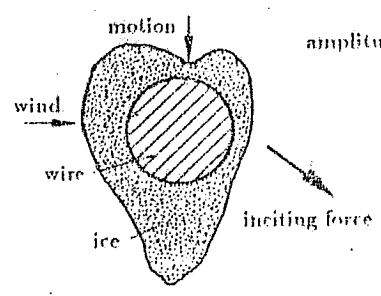
(a) viscous damping (fluid friction on the surface)



(b) Coulomb damping (solid friction on the surface)



(c) structural or hysteretic damping (internal friction of the material)



(d) negative damping (energy extracted from the fluid)

7.2) Amortecimento Viscoso:

"Força Viscosa" : $-\mu \dot{u}$

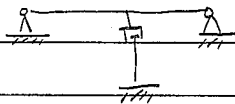
Potência Virtual associada : $\langle -\mu \dot{u}, v \rangle = - \int_{\mathcal{R}_e} \mu \dot{u} v \, dV$

Visão Discretizada : $-\sum_{i=1}^{ng} \int_{\mathcal{R}_e} \mu (\sum_i \dot{u}_i \psi_i) v$

Obtendo a matriz de amortecimento:

$$[C]_{ij} = \sum_{i=1}^{ng} \int_{\mathcal{R}_e} \mu \psi_i \psi_j \, dV$$

Obs: Caso em que a força viscosa não é distribuída, ex.



$$\Rightarrow M \ddot{u} + C \dot{u} + K u = F(t)$$

Problema: Como diagonalizar a eq. acima

alternative: $C = \alpha K + \beta M$

como escolher

$$D = X^T C X = \begin{bmatrix} d_1 & & \\ & \dots & \\ & & d_m \end{bmatrix}$$

onde $d_i = \left(\alpha + \frac{\beta}{\omega_i^2} \right) \omega_i^2$ coeficientes de amortecimento modal

Obs.: Ao invés da opção anterior podemos usar o reconhecimento do fator de amortecimento modal e, em seguida, a posterior obtenção de C através de $C = X^{(1)} D X^{-1}$

7.3) Amortecimento Estrutural

• Fenomenológico

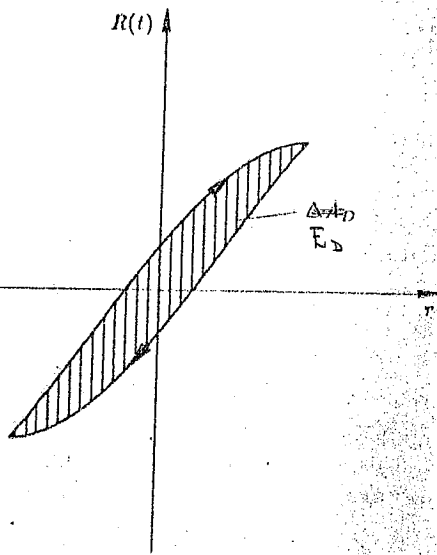


Fig. 1.4.6
Loss of energy due to damping:
R/r-diagram

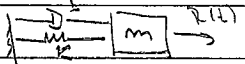
Amortecimento Estrutural observado através de excitação cíclica:

Regime permanente: Energia Gêdida = Energia Dissipada

$$E_D = \int_0^{T_E} R(t) \dot{u}(t) dt$$

\nearrow período \nearrow velocidade
 \nwarrow espaço de excitação

Fazendo: $R(t) = R_0 \sin \omega_E t \rightarrow u(t) = \frac{R_0}{k} V \sin(\omega_E t - \psi)$

Supondo  e V é o fator de amplificação

$$E_D = \frac{R_0^2}{k} V \omega_E \int_0^{T_E} \sin(\omega_E t) \cos(\omega_E t - \psi) dt = \frac{R_0^2}{k} V \omega_E \sin \psi$$

$$Z \gamma \omega = \frac{b}{m} = \frac{c}{k} \omega^2$$



$$E_D = \frac{R_0^2}{k} \sqrt{\pi Z \gamma} \left(\frac{\omega_E}{\omega} \right) V = \underbrace{b \pi \omega_E}_{\frac{R_0 V}{k}} \frac{m_{MAX}^2}{k}$$

Observado: $E_D \propto m_{MAX}^2$ (e não $\propto \omega_E$)

$$E_D = b_{EX} m_{MAX}^2 \quad (\text{EXPERIMENTAL})$$

Amorl. Estat \sim Amortecimento Viscoso

$$b_{eq} = \frac{b_H}{\pi \omega_E} \quad (\text{usar } b_{eq} \sim b)$$

Equação de movimento: $\ddot{u} + \gamma \frac{\omega}{\omega_E} \dot{u} + \omega^2 u = \frac{(\omega^2) R_0}{k} \sin \omega_E t$

$$\text{com } \gamma = \frac{b_H}{\pi k}$$



$\gamma \sim 0.05$ pl metais

• Caso Multidimensional

Considerando a excitação $R = a \sin \Omega t$

Resposta em regime permanente $u = d \sin(\Omega t - \psi)$

Assim um modelo de atrito viscoso condizente é

$$R_D = -C \dot{u} = -C d \Omega \cos(\Omega t - \psi) = f(\Omega)$$

\rightarrow ENERGIA Ω^2

$\} \text{Contradiz as observações experimentais!}$



Então $R_D = -\frac{1}{\Omega} C_d \dot{u}$



Assim, chegamos à equação:

$$M \ddot{u} + \frac{C_s}{\Omega} \dot{u} + K u = a \sin \Omega t$$

onde $\frac{C_s}{\Omega}$ corresponde à matriz calculada em (7.2).

Para evitar o uso de Ω na equação acima lança-se mão de uma formulação complexa:

$$M \ddot{u}_s + \frac{1}{\Omega} C_s \dot{u}_s + K u_s = a \sin \Omega t$$

$$M \ddot{u}_c + \frac{1}{\Omega} C_s \dot{u}_c + K u_c = a \cos \Omega t$$



Fazendo $\tilde{u} = u_c + j u_s$

$$M \ddot{\tilde{u}} + C_s \dot{\tilde{u}} + K \tilde{u} = a e^{j\Omega t} = \tilde{R}$$

Solução em regime permanente $\tilde{u} = \tilde{b} e^{j\Omega t}$

$$\dot{\tilde{u}} = j\Omega \tilde{b} e^{j\Omega t} = j\Omega \tilde{u}$$

Voltando à eq. diferencial

$$M \ddot{\tilde{u}} + [K + j C_s] \dot{\tilde{u}} = \tilde{R}(t)$$

$$C_s \sim K$$

$$M \ddot{\tilde{u}} + (1 + jg) K \tilde{u} = \tilde{R}(t)$$

$$g \leq 0.05 \quad (\text{pl metais})$$



Logo

$$[C]_{ij} = -\frac{1}{\omega_d^2} \int_{\Omega} \mathcal{R}_k \cdot \sigma_i^d$$

7.4) Resposta Dinâmica de sistemas com Amortecimento Modal

⇒ Análise Espectral do Sistema Conservativo Associado

$$A \ddot{q} + D \dot{q} + q = R_q(t) \quad (D \dots \text{diagonal})$$

$$\rightarrow \ddot{q}_i + 2 \zeta_i \omega_i \dot{q}_i + \omega_i^2 q_i = \omega_i^2 R_{qi}$$

$$\zeta_i = \frac{w_i d_i}{2}$$

Inicialmente $R_{qi}(t) = 0$

$$\rightarrow \ddot{q}_i + 2 \zeta_i \omega_i \dot{q}_i + \omega_i^2 q_i = 0$$

$$\eta_i(t) = e^{-\omega_i \zeta_i t} (a_i \sin \omega_{Di} t + b_i \cos \omega_{Di} t)$$

if $\zeta_i < 1$ (sub-critical)

$$\eta_i(t) = (a_i + b_i t) e^{-\omega_i t}$$

if $\zeta_i = 1$ (critical)

$$\eta_i(t) = a_i e^{-\omega_i(\zeta_i - \sqrt{\zeta_i^2 - 1})t} + b_i e^{-\omega_i(\zeta_i + \sqrt{\zeta_i^2 - 1})t}$$

if $\zeta_i > 1$ (over-critical)

$$\text{Com } \omega_{Di} = \omega_i \sqrt{1 - \zeta_i^2}$$

Para o sistema sub-crítico

$$\eta_i = e^{-\omega_i \zeta_i t} \left(\frac{\dot{\eta}_{0i} + \omega_i \zeta_i \eta_{0i}}{\omega_i \sqrt{1 - \zeta_i^2}} \sin \omega_i \sqrt{1 - \zeta_i^2} t + \eta_{0i} \cos \omega_i \sqrt{1 - \zeta_i^2} t \right)$$

$$= e^{-\omega_i \zeta_i t} \left(\frac{\dot{\eta}_{0i} + \omega_i \zeta_i \eta_{0i}}{\omega_{Di}} \sin \omega_{Di} t + \eta_{0i} \cos \omega_{Di} t \right)$$

• Excitação não nula:

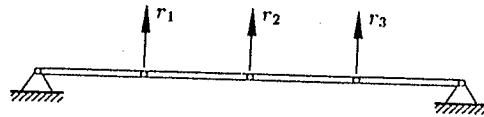
$$q_i(t) = e^{-\gamma_i t} (a_i \sin \omega_i t + b_i \cos \omega_i t) + q_i^p(t)$$

(amortecimento sub-crítico)

• Mesmo tratamento que no caso sem amortecimento levando à

$$F_i = \frac{1}{1 - \left(\frac{\Omega}{\omega_i}\right)^2 + j 2 \zeta_i \left(\frac{\Omega}{\omega_i}\right)} \Rightarrow V_i = \left(\left[1 - \left(\frac{\Omega}{\omega_i}\right)^2 \right]^2 + \left[2 \zeta_i \left(\frac{\Omega}{\omega_i}\right) \right]^2 \right)^{-1/2}$$

$$\text{e } \varphi_i = \tan^{-1} \frac{2 \zeta_i \Omega / \omega_i}{1 - (\Omega / \omega_i)^2} \Rightarrow q_i^p = V_i (\cos(\Omega t - \varphi_i) + j \sin(\Omega t - \varphi_i))$$



$$x_2 = \{1 \ 0 \ 1\}$$

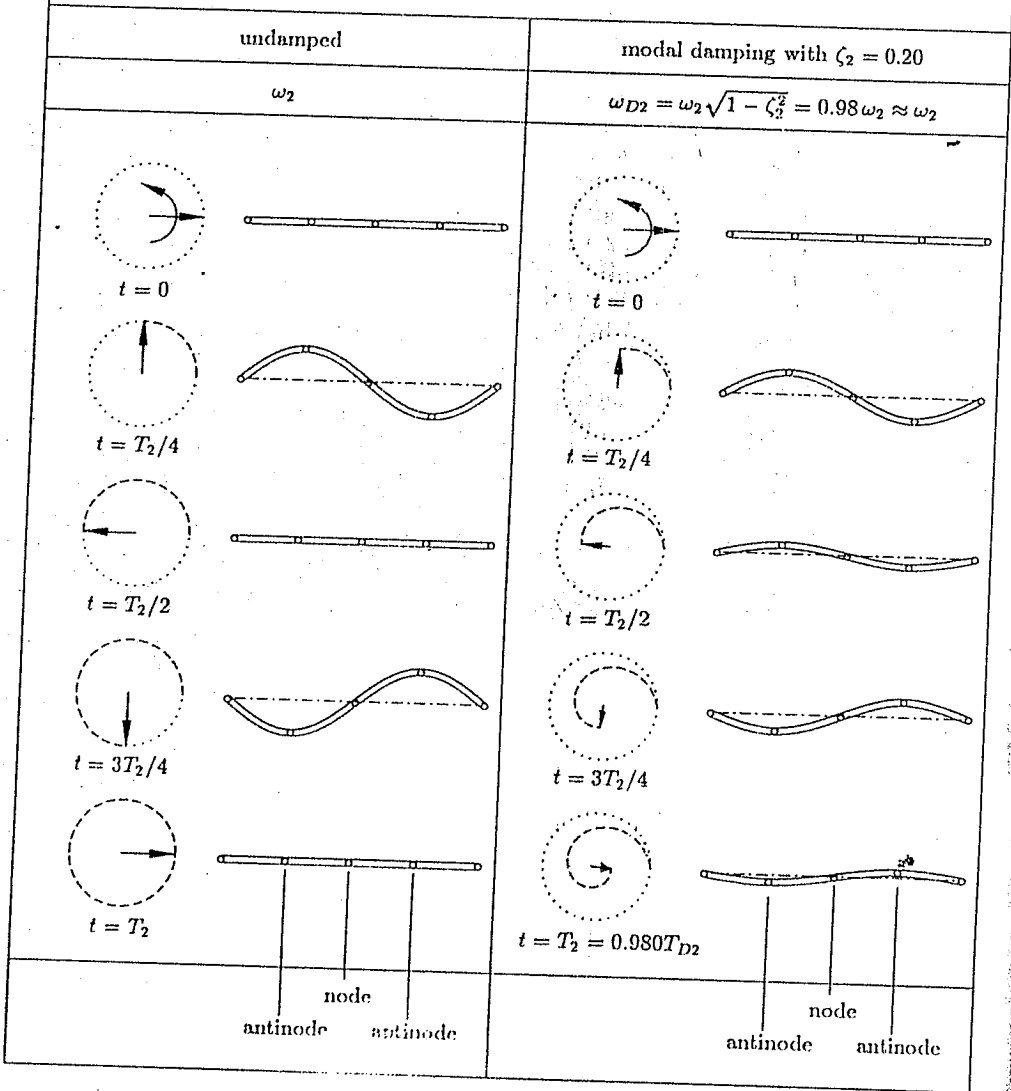


Fig. 7.4.1 Undamped and modally damped eigenoscillations for identical initial conditions recorded at the same instant t